

April 8, 2022

Santa Rosa County School District 6544 Firehouse Road Milton, Florida 32570

Attn: Mr. Joseph B. Harrell

Assistant Superintendent for Administrative Services

Subject: Preliminary Geotechnical Engineering Report

SRCSD S.A. JONES ROAD SITE
Milton, Santa Rosa County, Florida
NOVA Project Number 10116-2022037

Dear Mr. Harrell:

NOVA Engineering and Environmental LLC (NOVA) has completed the authorized <u>Preliminary</u> Geotechnical Engineering Report for the potential school campus to be located near Milton in unincorporated Santa Rosa County, Florida. The work was performed in general accordance with NOVA Proposal Number 016-20229646, dated February 11, 2022. This report briefly discusses our understanding of the project at the time of the subsurface exploration, describes the geotechnical consulting services provided by NOVA, and presents our <u>preliminary</u> findings, conclusions, and recommendations.

The primary objective of this study was to provide a preliminary geotechnical exploration of the near surface soils within potential foundation, pavement, and stormwater management system (SMS) areas across the area of study. The authorized preliminary geotechnical engineering services included performing two (2) Standard Penetration Test (SPT) borings (designated B-1 and B-2), each drilled to depth of about 25 feet below existing grade (BEG); four (4) auger borings (A-1 through A-4) drilled to depths of roughly $5\frac{1}{2}$ feet to 10 feet BEG (some of the test borings encountered refusal due to the presence of iron rock); and one (1) 35-foot deep SPT boring (S-1) drilled within the most likely proposed stormwater management system (SMS) area.

Project Description

We understand that the proposed development could potentially include constructing a twostory school building with associated paved entrance drives and parking areas and a Stormwater Management System (SMS) to treat and dispose of stormwater runoff. Given the property's location, we anticipate that the SMS will most likely need to be a dry retention basin constructed with an underlying vertical sand chimney.

Site Location and Description

The proposed educational facility is proposed to be located along the west side of S.A. Jones Road, south of Interstate 10, several miles east of Milton in unincorporated Santa Rosa County, Florida. The parcel is identified by the Santa Rosa County Property Appraiser as parcel ID 35-2N-27-0000-00100-0000. A Site Location Map is included in Appendix A.

At the time of our preliminary field exploration, the area of study consisted primarily of vacant timberland which had been harvested within the last 5-10 years, as well as delineated wetlands located near the northeast property corner. The Subject Property was observed to be gently sloping away from the north-south centerline. The site was bordered by Interstate 10 to the north, S.A. Jones Road to the east, and mixed residential and timberland uses to the south and west.

Subsurface Conditions

As noted above, our field exploration at the subject site included performing three (3) Standard Penetration Test (SPT) borings to depths of about 25 feet (2 borings) and 35 feet (1 boring) below existing grade (BEG) and four (4) auger borings to depths varying between roughly $5\frac{1}{2}$ feet to 10 feet BEG. Drilling, testing and sampling operations were performed in general accordance with ASTM designations and other industry standards. The Test Boring Records and a summary of laboratory soil testing results are provided in the attached Appendix.

Beneath up to 6 inches of topsoil, the test borings generally encountered mixed strata of very loose to medium dense fine-grained slightly silty to clayey sands (USCS classifications of SP-SM, SM, and SC), with embedded iron rock fragments at variable depths in some borings, to a depth of about 25 BEG underlain by medium dense fine- to medium-grained sands (SP) to the maximum depth explored of approximately 35 feet BEG.

We note that Test Boring A-2 was terminated at a depth of about $5\frac{1}{2}$ feet BEG due to groundwater intrusion, and Test Borings A-1 and A-4 were terminated at depths of roughly 7 feet and $7\frac{1}{2}$ feet, respectively, after encountering refusal due to the presence of iron rock.

A stabilized groundwater table was encountered in Test Boring A-2 at a depth of about $3\frac{1}{2}$ feet BEG (we note that this boring was located adjacent to a wetland present in the northeastern portion of the site), and was not encountered within the maximum depths explored of roughly 7 feet to 35 feet BEG in the remainder of the test borings at the time of our field exploration, which occurred during a period of relatively normal seasonal rainfall and shortly following the passing of several significant rain events.

Based on comparisons of current annual monthly rainfall data to historical rainfall data extending back 50+ years in time, we estimate that the normal permanent seasonal high groundwater (SHGW) table for this site will occur within 1 foot above the measured depth to groundwater at the Test Boring A-2 location, and will remain below the maximum depths



explored for the other borings. We note that groundwater levels vary with changes in season and rainfall, construction activity, surface water runoff and other site-specific factors. Groundwater levels in the northern Santa Rosa County area are typically lowest in the late fall to winter and highest in the early spring to mid-summer with annual groundwater fluctuations by seasonal rainfall; consequently, the water table may vary at times.

Preliminary Site Discussion

The following preliminary conclusions and design considerations are based on our understanding of the proposed development, our site observations, our evaluation and interpretation of the field and laboratory data obtained during this exploration, our experience with similar subsurface conditions in the region, and generally accepted geotechnical engineering principles and practices.

Based on the results of our field exploration, the subsurface conditions encountered beneath this site (to the maximum depth drilled of about 35 feet BEG) appear to be feasible employing conventional site preparation practices.

The near surface soils, excluding topsoil, consisted of very loose to loose fine-grained slightly silty to silty sands which should be suitable for reuse as structural fill for this project after they have been properly compacted. However, we note that strict moisture control will be required at the time of placement for these moisture-sensitive soils.

Although groundwater is not expected to impact the development of this property, maintaining proper grades (i.e., positive drainage paths) during the construction phase of this project will be critical to avoid the development of "bird baths" within the construction areas, which would degrade the underlying silty soils and require undercutting to more firm underlying soils.

A further, more extensive, geotechnical exploration should be performed in proposed structure and pavement areas after a Site Plan has been established for this project.

Structures

Shallow spread footing foundations for the planned school structure(s) should be appropriate with the employment of "typical" site preparation operations. A design soil bearing pressure on the order of **1,500** to **2,500** psf should be obtainable for the planned building foundations, depending on the type/size of construction equipment utilized during the site preparation phase of construction.

The higher bearing pressure noted above is achievable with improvement of the very loose to loose subgrade soils encountered in the upper 4 to 6 feet of the soil horizon in the test borings, which can typically be accomplished from the stripped grade elevation using a large, ride-on vibratory roller (i.e., a minimum 10-ton steel wheel roller, static weight, with a minimum 5-foot drum diameter) if these soils are not found to be overly wet once site preparation activities have begun.



Pavements

Typical asphalt pavement sections designed for a 20-year design life should be appropriate for this site with the employment of "typical" site preparation operations.

<u>Preliminary SMS Design Considerations</u>

NOVA understands that a stormwater management system consisting of a shallow dry retention basin is desired for the treatment and disposal of stormwater runoff associated with the planned improvements to the property. Based upon the results of the test borings, the subsurface conditions encountered appear (preliminarily, subject to confirmation of the soil conditions and design parameters presented herein with borings performed within the actual SMS footprint once a proposed Site Plan is available) to be unsuitable for employing this desired SMS due to the presence of the low-permeability silty to clayey sands encountered at and extending well below the anticipated pond bottom elevation.

However, the SMS appears to be adaptable for employing a shallow basin with an underlying sand chimney feature designed to intercept the deeper, more permeable sand strata encountered in the deeper SPT borings beginning at about 21 feet BEG. We note that difficult digging conditions should be expected due to the presence of iron rock at variable depths beneath this property. We recommend that you consider the soil parameters presented below for a preliminary design of the SMS at the subject project site.

Table 1 -Preliminary SMS Soil Design Parameters		
Estimated Depth to Confining Stratum, BEG Assuming a sand chimney is constructed beneath the basin bottom as recommended herein, and cannot exceed the maximum depth explored on the site.	Below 35 feet	
Measured Vertical Hydraulic Conductivity Rate at Chimney Bottom (Kv)	41 feet/day	
Calculated Horizontal Hydraulic Conductivity at Chimney Bottom (Kh)	62 feet/day	
Estimated In-Situ Infiltration Rate (DRI)	14 inches/hour	
Maximum Area for Unsaturated Infiltration (ft^2) – to be determined by designer, based on the but the value must equal the chimney footprint.	outflow required,	
Estimated Embedment Depth for Vertical Sand Chimney to Key Into Underlying More Permeable Strata, BEG	23 feet	
Estimated Depth of Seasonal High Groundwater Table, BEG	Below 35 feet	

We note that the provided parameters presented in the table above are unfactored.

Once a site design has been established for the project, a more comprehensive SMS evaluation should be conducted to establish confining strata depths as well as estimated seasonal high and low groundwater tables for the proposed basin(s).



Conclusion

We appreciate your selection of NOVA and the opportunity to be of service on this project. If you have any questions, or if we may be of further assistance, please do not hesitate to contact us.

Sincerely,

NOVA Engineering and Environmental LLC

Jesse A. James P.E. Assistant Branch Manager Florida Registration No. 90470 William L. Lawrence, P.E. Senior Regional Engineer

Florida Registration No. 60147



APPENDIX A Figures and Maps



Scale: Not To Scale

Date Drawn: March 17, 2022

Drawn By: C.Pickett
Checked By: J.James



140-A Lurton Street Pensacola, Florida 32505 850.607.7782 ♦ 850.249.6683

PROJECT LOCATION MAP

SRCSD S.A. Jones Road Site Milton, Santa Rosa County, Florida NOVA Project Number 10116-2022037



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Points

Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

... Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot
Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

LOLIND

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

Special Line Features

Water Features

Δ

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Santa Rosa County, Florida Survey Area Data: Version 18, Sep 13, 2021

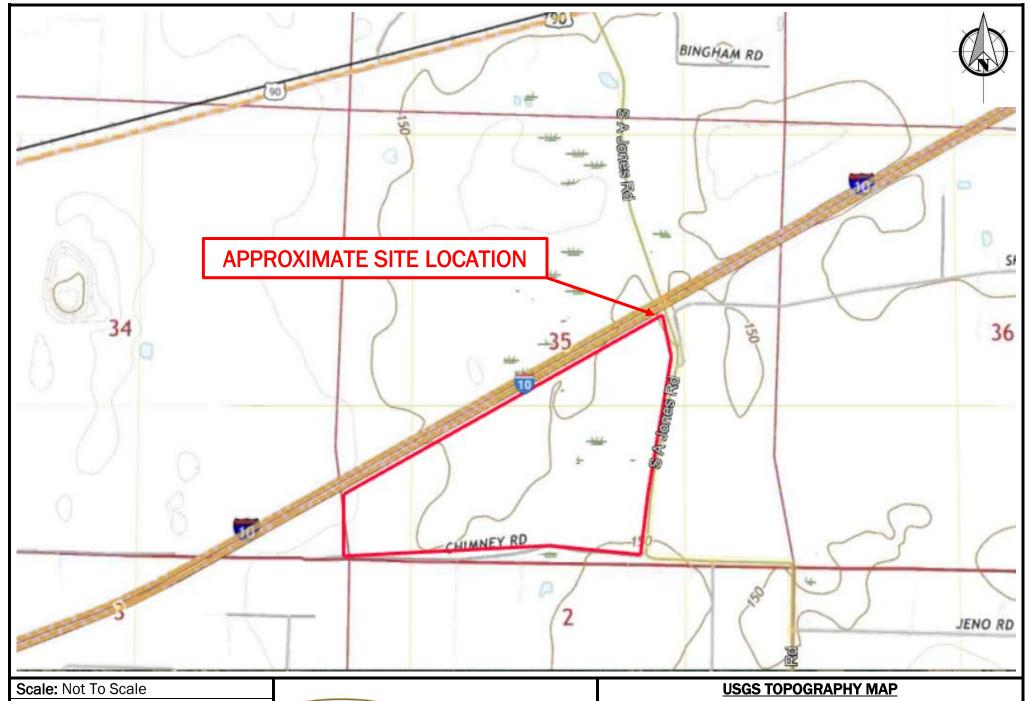
Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Dec 31, 2009—Nov 2, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
14	Fuquay loamy sand, 0 to 5 percent slopes	5.0	3.3%
21	Lakeland sand, 0 to 5 percent slopes	57.1	37.8%
40	Rutlege loamy sand	8.0	5.3%
44	Troup loamy sand, 0 to 5 percent slopes	81.1	53.6%
Totals for Area of Interest	,	151.2	100.0%



Date Drawn: March 17, 2022

Drawn By: C.Pickett
Checked By: J.James



140-A Lurton Street Pensacola, Florida 32505 850.607.7782 ♦ 850.249.6683 SRCSD S.A. Jones Road Site
Milton, Santa Rosa County, Florida
NOVA Project Number 10116-2022037

APPENDIX B Subsurface Data



LEGEND

B-x = 25-ft. SPT Boring

S-x = 35-ft SMS SPT Boring

• A-x = 10-ft Auger Boring

Scale: Not To Scale

Date Drawn: March 3, 2022

Drawn By: J. James

Checked By: W. Lawrence



140-A Lurton Street Pensacola, Florida 32505 850.607.7782 ◆ 850.249.6683 BORING LOCATION PLAN
SRCSD S.A. Jones Site
Milton, Santa Rosa County, Florida
NOVA Project Number 10116-2022037



KEY TO BORING LOGS

SYMBOLS AND ABBREVIATIONS SYMBOL DESCRIPTION No. of Blows of a 140-lb. Weight Falling 30 N-Value Inches Required to Drive a Standard Spoon WOR Weight of Drill Rods WOH Weight of Drill Rods and Hammer Sample from Auger Cuttings Standard Penetration Test Sample Thin-wall Shelby Tube Sample (Undisturbed Sampler Used) % REC Percent Core Recovery from Rock Core Drilling RQD Rock Quality Designation Stabilized Groundwater Level Seasonal High Groundwater Level (also referred to as the W.S.W.T.) NE Not Encountered **GNE** Groundwater Not Encountered BT **Boring Terminated** -200 (%) Fines Content or % Passing No. 200 Sieve MC (%) Moisture Content

UNIFIED SOIL CLASSIFICATION SYSTEM

MAJOR DIVISIONS GROUP			
MAJOR DIVIS	SIONS	GROUP SYMBOLS	TYPICAL NAMES
GRAVELS	CLEAN	GW	Well-graded gravels and gravel- sand mixtures, little or no fines
50% or more of	GRAVELS	GP	Poorly graded gravels and gravel-sand mixtures, little or no fines
fraction retained on	GRAVELS	GM	Silty gravels and gravel-sand- silt mixtures
No. 4 sieve	WITH FINES	GC	Clayey gravels and gravel- sand-clay mixtures
GRAVELS S0% or more of coarse fraction retained on No. 4 sieve GRAVELS GP		Well-graded sands and gravelly sands, little or no fines	
More than 50% of	0.000.000.000.000.000.000.000	SP**	Poorly graded sands and gravelly sands, little or no fines
fraction passes No.	SANDS with 12% or more	SM**	Silty sands, sand-silt mixtures
4 sieve	passing No. 200 sieve	SC**	Clayey sands, sand-clay mixtures
		ML	Inorganic silts, very fine sands, rock flour, silty or clayey fine sands
Liqu	id limit	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, lean clays
g.		OL	Organic silts and organic silty clays of low plasticity
		МН	Inorganic silts, micaceous or diamicaceous fine sands or silts, elastic silts
Liqu	id limit	СН	Inorganic clays or clays of high plasticity, fat clays
greater	than 50%	ОН	Organic clays of medium to high plasticity
		PT	Peat, muck and other highly organic soils
	GRAVELS 50% or more of coarse fraction retained on No. 4 sieve SANDS More than 50% of coarse fraction passes No. 4 sieve SILTS Al Liqu 50%	SANDS More than 50% of coarse fraction retained on No. 4 sieve SANDS More than 50% of coarse fraction passes No. 4 sieve GRAVELS WITH FINES CLEAN SANDS 5% or less passing No. 200 sieve SANDS with 12% or more passing No.	GRAVELS 50% or more of coarse fraction retained on No. 4 sieve GRAVELS More than 50% of coarse fraction passes No. 4 sieve SILTS AND CLAYS Liquid limit greater than 50% GRAVELS WITH FINES GRAVELS GM GRAVELS WITH FINES GC CLEAN SANDS 5% or less passing No. 200 sieve SANDS with 12% or more passing No. 200 sieve CLEAN SANDS WITH SM** SP** SM** SM** SM** SM** SM** CL MH SILTS AND CLAYS Liquid limit greater than 50% OH

*Based on the material passing the 3-inch (75 mm) sieve
*** Use dual symbol (such as SP-SM and SP-SC) for soils with more

than 5% but less than 12% passing the No. 200 sieve

RELATIVE DENSITY

Coefficient of Permeability

Ground Surface Elevation

Organic Content

Liquid Limit (Atterberg Limits Test)

Plasticity Index (Atterberg Limits Test)

LL

PI

K

Org. Cont.

G.S. Elevation

(Sands and Gravels)
Very loose – Less than 4 Blow/Foot
Loose – 4 to 10 Blows/Foot
Medium Dense – 11 to 30 Blows/Foot
Dense – 31 to 50 Blows/Foot
Very Dense – More than 50 Blows/Foot

CONSISTENCY

(Silts and Clays)

Very Soft – Less than 2 Blows/Foot
Soft – 2 to 4 Blows/Foot

Medium Stiff – 5 to 8 Blows/Foot
Stiff – 9 to 15 Blows/Foot
Very Stiff – 16 to 30 Blows/Foot
Hard – More than 30 Blows/Foot

RELATIVE HARDNESS

(Limestone)
Soft – 100 Blows for more than 2 Inches
Hard – 100 Blows for less than 2 Inches

MODIFIERS

These modifiers Provide Our Estimate of the Amount of Minor Constituents (Silt or Clay Size Particles) in the Soil Sample

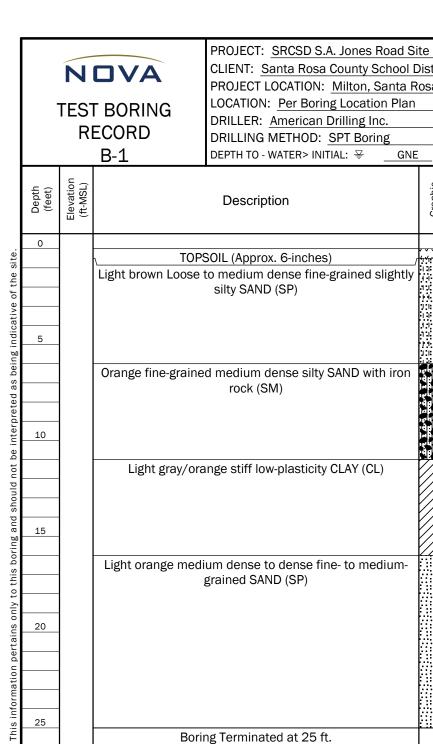
Trace – 5% or less
With Silt or With Clay – 6% to 11%
Silty or Clayey – 12% to 30%
Very Silty or Very Clayey – 31% to 50%

These Modifiers Provide Our Estimate of the Amount of Organic Components in the Soil Sample

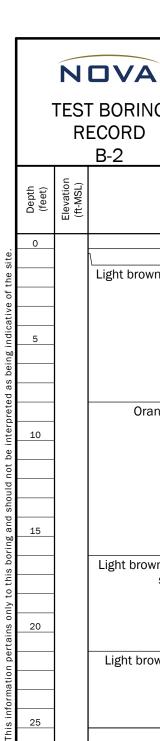
Trace – Less than 3% Few – 3% to 4% Some – 5% to 8% Many – Greater than 8%

These Modifiers Provide Our Estimate of the Amount of Other Components (Shell, Gravel, Etc.) in the Soil Sample

Trace – 5% or less Few – 6% to 12% Some – 13% to 30% Many – 31% to 50%



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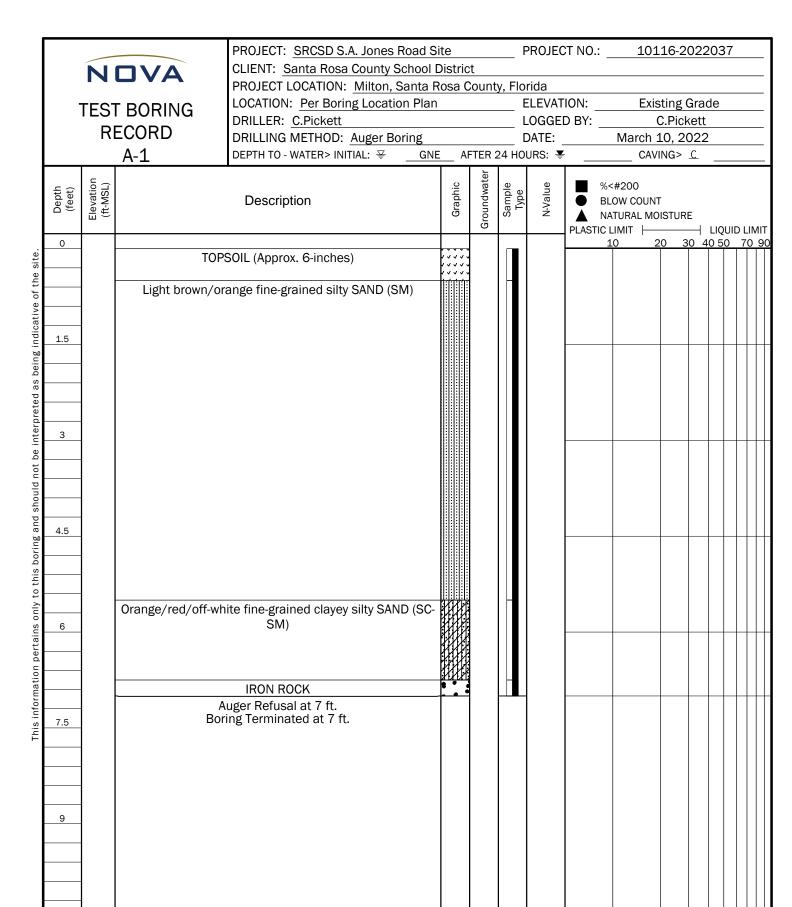


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JVA	PROJECT LOCATION: Milton, Santa F			y, Flor	ida						_
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Light brown/ora	ange medium dense fine- to medium- grained SAND (SP)				25						
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*NOTE: Elevation was approximated utilizing USGS Topography.

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-86.92327466



*NOTE: Auger refusal at 7 ft. due to iron rock layer

10.5



TEST BORING RECORD

This information pertains only to this boring and should not be interpreted as being indicative of the site.

PROJECT: SRCSD S.A. Jones Road Site PROJECT NO.: 10116-2022037 CLIENT: Santa Rosa County School District PROJECT LOCATION: Milton, Santa Rosa County, Florida LOCATION:Per Boring Location PlanELEVATION:Existing GradeDRILLER:C.PickettLOGGED BY:C.Pickett DRILLING METHOD: Auger Boring DATE: March 10, 2022

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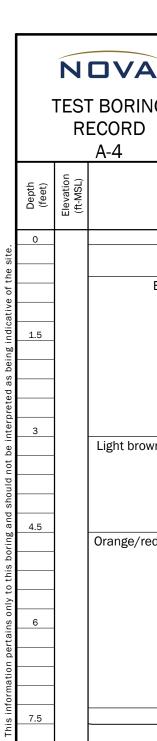


TEST BORING RECORD

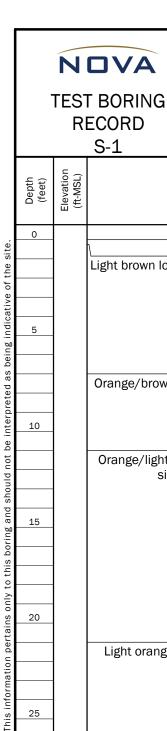
This information pertains only to this boring and should not be interpreted as being indicative of the site.

PROJECT: SRCSD S.A. Jones Road Site PROJECT NO.: 10116-2022037 CLIENT: Santa Rosa County School District PROJECT LOCATION: Milton, Santa Rosa County, Florida LOCATION:Per Boring Location PlanELEVATION:Existing GradeDRILLER:C.PickettLOGGED BY:C.Pickett DRILLING METHOD: Auger Boring DATE: March 10, 2022

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			PROJECT LOCATION: Milton, Santa					_					_
7	TES1	ΓBORING	LOCATION: Per Boring Location Plan			E	LEVATI	ON:	Existi	ng Gra	ade		_
		ECORD	DRILLER: C.Pickett			<u>L</u>	OGGEE) BY:	C.I	Picket	<u>:t</u>		-1
	1 \ 1		DRILLING METHOD: Auger Boring										-1
		A-4	DEPTH TO - WATER> INITIAL: ♀ GN	E Al	- IER :	24 HOU	JRS: 뵺		CAVIN	G> <u>L</u>	_		_
Depth (feet)	Elevation (ft-MSL)		Description	Graphic	Groundwater	Sample Type	N-Value	● BLC	#200 DW COUNT FURAL MOIS MIT		LIOU	ID LII	MIT
0										30			
		TOP	SOIL (Approx. 6-inches)	7777									
			CAND (OM)										
		Brown fi	ne-grained silty SAND (SM)										$ \cdot $
													$ \cdot $
1.5													$ \cdot $
							ŀ			\top		$\dagger \dagger$	$\dagger \dagger \dagger$
													$ \cdot $
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													Ш
3		1 : db t b /	co fine a speciment of the control o				-			-			+
		Light brown/orang	ge fine-grained slightly silty SAND (SP- SM)	7:000									Ш
			Sivi)	13061									Ш
			73.671									Ш	
				11000									Ш
4.5				1:1:1:1:1									
		Orange/red/off-wh	ite fine-grained clayey silty SAND (SC										
			SM)										Ш
													Ш
6													Ш
												\top	Ш
													Ш
													$ \cdot $
			IRON ROCK	INN									$ \cdot $
7.5		Λ.	iger Refusal at 7.5 ft.	 • •			ŀ			+	+	+	┼┼┨
		Borii	ng Terminated at 7.5 ft.										$ \cdot $
			-										$ \cdot $
													$ \cdot $
													$ \cdot $
9													$ \cdot $
													$ \cdot $
													$ \cdot $
													$ \cdot $
													$ \cdot $
10.5													$ \cdot $
													$ \cdot $
*NOTE:	Auger	refusal at 7.5 ft. due to ir	ron rock layer	•									



PROJECT: SRCSD S.A. Jones Road Site PROJECT NO.: 10116-2022037 CLIENT: Santa Rosa County School District PROJECT LOCATION: Milton, Santa Rosa County, Florida LOCATION: Per Boring Location Plan ELEVATION: *150 ft. NAVD88 DRILLER: American Drilling Inc. LOGGED BY: ____ C.Pickett DRILLING METHOD: SPT Boring March 28, 2022 DATE: DEPTH TO - WATER> INITIAL: ¥ GNE AFTER 24 HOURS: 🐺 CAVING> C

		<u> </u>					
Depth (feet)	Elevation (ft-MSL)	Description	Graphic	Groundwater	Sample Type	N-Value	
0							10 20 30 40 50 70 90
		TOPSOIL (Approx. 3-inches)	11111			8	7
		Light brown loose fine-grained slightly silty SAND (SP-SM)	19 (1.6				
		Light brown loose line grained slightly slity shirts (or slith)	19:11			1	
			111.01.0			4	
							<u> </u>
						4	•
5			min				
						_	<u> </u>
			1100000			7	
		Orange/brown loose to medium dense fine-grained silty					
		SAND (SM)				14	•
		- (- /					
10							
		Orange/light brown medium dense fine-grained clayey					
		silty SAND with iron rock (SC-SM)					
		· · · · · · · · · · · · · · · · · · ·				17	•
15							
						19	
						19	I
20							
					_		
		Light orange/brown medium dense to dense fine- to	L YELL				
		medium-grained SAND (SP)					
		mediani-grained SAND (SI)					
						19	I –
25							
			 			22	-
20			:::::::				
30					🆳		
			ļi.i				
			::::::			31	
35		Paring Tarminated at 25 ft	:::::		H		
		Boring Terminated at 35 ft.					
*NOTE:	Elevati	on was approximated utilizing USGS Topography.					

30.63065480 -86.92635447

APPENDIX C Laboratory Data

SUMMARY OF CLASSIFICATION & INDEX TESTING

SRCSD S.A. Jones Road Site

Milton, Santa Rosa County, Florida NOVA Project No. 10116-2022037

	SUMMARY OF CLASSIFICATION AND INDEX TESTING												
	Sample	Natural	Percent	Hyd	draulic Conductivity	USCS							
Boring No.	Depth (ft. BEG)	Moisture (%)	Fines (- #200)	K _{vs} (ft/day)	Unit Weight of Sample (pcf)	Soil Classification							
A-2	0.5-2.5	15	16			SM							
A-2	4-5	18	32			SM							
A-3	0.5-3.5	6	10			SP-SM							
A-3	3.5-5	5	7			SP-SM							
B-1	4-6	7	12			SP-SM							
B-1	8-10	16	29			SM							
B-1	13-15	20	63			CL							
B-1	18-20	5	5			SP							
B-2	13-15	11	19			SM							
B-2	18-20	15	29			SC-SM							
B-2	23-25	5	4			SP							
S-1	22-28	4	3	41	SP								
S-1	28-33	3	2			SP							



REMOLDED LABORATORY PERMEABILITY TEST DATA SHEET

PROJECT:	SRCSD S.A. Jones Site	NOVA PROJECT #:		10116-2022037		
•						
DATE:	3/28/2022	ASSIGNED BY:	J.James	TESTED BY:	C.Pickett	

Sample LOCATION / BORING NO.	S-1
Sample NUMBER / DEPTH	22-28 ft.

FALLING HEAD PERMEABILITY (ASTM D 5084)					
No. of LAYERS:		3	Wt. of MOLD (lbs):		4.48
BLOWS/LAYER:		15	Wt. of MOLD/SOIL (lbs):		7.97
HEIGHT (FT)	TRIAL #1 (SEC)		PERMEABILITY		
7	0.0		1.54E-02		
6	0.9			1.37E-02	
5	2.2			1.3	4E-02
4	3.8			1.4	7E-02
3	6.0		1.57E-02		
2	8.9				
1	12.6				
1.5E-02 cm/sec					cm/sec

PERMEABILITY TESTING SUMMARY						
PERMEABILITY (K _V)	\rightarrow	41	ft/day			
Corresponding K _h	\rightarrow	62	ft/day			
DRY DENSITY	\rightarrow	101	lbs/ft ³			
MOISTURE CONTENT	\rightarrow	4	%			
-200 FINES CONTENT	\rightarrow	3	%			

MOISTURE CONTENT (ASTM D 2216)				
Pan NUMBER	R			
Wt. of WET SOIL & PAN (g)	237.1			
Wt. of DRY SOIL & PAN (g)	230.4			
Wt. of PAN (g)	65.2			
Wt. of Water (g)	6.7			
Wt. of Dry Soil (g)	165.2			
MOISTURE CONTENT (%)	4.1			

-200 SIEVE WASH (ASTM D 1140)				
Pan NUMBER	R			
Wt. of DRY SOIL & PAN (g)	230.4			
Wt. of WASH SOIL & PAN (g)	225.3			
Wt. of PAN (g)	65.2			
Wt. of Original Dry Sample (g)	165.2			
Wt. of -200 Material (g)	5.1			
Wt. of Washed Dry Sample (g)	160.1			
-200 FINES CONTENT (%)	3.1			

NUMBER OF INCHES MOLD WAS SHORT? PERMEABILITY CONSTANT USED WAS \rightarrow

0.000 INCHES (ZERO INCHES IS DEFAULT)

0.23 (Includes 3/8"ID tubing)



APPENDIX D Qualifications of Recommendations

QUALIFICATIONS OF RECOMMENDATIONS

The findings, conclusions and recommendations presented in this report represent our professional opinions concerning subsurface conditions at the site. The opinions presented are relative to the dates of our site work and should not be relied on to represent conditions at later dates or at locations not explored. The opinions included herein are based on information provided to us, the data obtained at specific locations during the study, and our previous experience. If additional information becomes available which might impact our geotechnical opinions, it will be necessary for NOVA to review the information, re-assess the potential concerns, and re-evaluate our conclusions and recommendations.

Regardless of the thoroughness of a geotechnical exploration, there is the possibility that conditions between borings may differ from those encountered at specific boring locations, that conditions are not as anticipated by the designers and/or the contractors, or that either natural events or the construction process has altered the subsurface conditions. These variations are an inherent risk associated with subsurface conditions in this region and the approximate methods used to obtain the data. These variations may not be apparent until construction.

The professional opinions presented in this report are not final. Field observations and foundation installation monitoring by the geotechnical engineer, as well as soil density testing and other quality assurance functions associated with site earthwork and foundation construction, are an extension of this report. Therefore, NOVA should be retained by the owner to observe all earthwork and foundation construction to confirm that the conditions anticipated in this study actually exist, and to finalize or amend our conclusions and recommendations. NOVA is not responsible or liable for the conclusions and recommendations presented in this report if NOVA does not perform these observations and testing services.

This report is intended for the sole use of **Santa Rosa County School District** only. The scope of work performed during this study was developed for purposes specifically intended by of **Santa Rosa County School District** only and may not satisfy other users' requirements. Use of this report or the findings, conclusions or recommendations by others will be at the sole risk of the user. NOVA is not responsible or liable for the interpretation by others of the data in this report, nor their conclusions, recommendations or opinions.

Our professional services have been performed, our findings obtained, our conclusions derived and our recommendations prepared in accordance with generally accepted geotechnical engineering principles and practices in the State of Florida. This warranty is in lieu of all other statements or warranties, either expressed or implied.

Important Information about This

Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical-engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one* — *not even you* — should apply this report for any purpose or project except the one originally contemplated.

Read the Full Report

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a lightindustrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.

Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. Do not rely on a geotechnical-engineering report whose adequacy may have been affected by: the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. Contact the geotechnical engineer before applying this report to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. Confirmation-dependent recommendations are not final, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations only by observing actual subsurface conditions revealed during construction. The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.

A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk*.

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, but preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/ or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure constructors have sufficient time* to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help

others recognize their own responsibilities and risks. *Read these provisions closely*. Ask questions. Your geotechnical engineer should respond fully and frankly.

Environmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical-engineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures*. If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else*.

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold- prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical- engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with you GBC-Member geotechnical engineer for more information.



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